

Design of the "Magnetic Platform" for the ITER in-vessel magnetic diagnostics

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Abstract

The "In-Vessel Magnetic platform" is a subsystem of the magnetic diagnostics formed by all the components necessary for the thermo-mechanical interface of the actual magnetic sensors with the Vacuum Vessel (VV), their protection and the electrical connection to the in-vessel wiring for the transmission of the detected signal with a minimum level of noise.

Significant efforts have been dedicated to integrate the CAD model within the ITER In-Vessel configuration model, taking care of the geometrical compliance with the Blanket modules and the remote handling compatibility.

Thorough thermo-mechanical and electro-magnetic FEM analyses have been performed to assess the reliability of the system in standard and off-normal operating conditions.

Rationale of the design			f the design	Sensor location
	Flexible and Modular		House the different types of sensors	Several hundreds of magnetic sensors are required in ITER for machine protection, plasma control, equilibrium reconstruction and physics studies.
	Thermo Mech.		Fit in different positions on the VV	Located within the ITER VV, in a hostile environment characterized by severe neutron irradiation and plasma heat loads strongly affecting their reliability and durability.
ments st)		Mechanical attachment to the VV	Efficient heat transfer to the VV	Attached to the inner surface of the VV, behind Blanket modules or divertor cassettes, through a connection system which allows a potential replacement by a suitable RH system.
			(passively cooled through thermal contact with the VV)	The "In-Vessel Magnetic Platform" is a component shared by a subset of the ITER in-vessel discrete magnetic
ire ^{ntra}				sensors: Inner Tangential Coils (55.AA), Inner Normal Coils (55.AB), Toroidal Coils (55.AC) and High Frequency Sensors
<mark>nt requ</mark> en in cor	E	Electrical connection to the in-vessel wiringEMI shielding from Electron Cyclotron Heating (ECH) stray radiation	(55.AJ).	
			Heating (ECH) stray radiation	The platform provides two main functions:
			• mochanical support within the $\frac{1}{1}$	



> Several thermo-mechanical and electromagnetic FEM analyses have been performed to assess various configuration of platform design considering different geometries and materials.

Thermal analysis

Detailed analyses on sensor and clamping

Dedicated FEM analyses to investigate the thermal gradient across the LTCC sensor in order to estimate and limit the level of TIEMF noise signal

Thermal analyses on whole assembly

Aim: Base Plate optimization for minimizing the thermal gradient between Base Plate and VV in the expected operating conditions. Several analyses for testing:

- different geometries of the groove;
- different welding configurations (2 or 4 welds);





- mechanical support within the vv;
- electrical connection to the in-vessel wiring for the transmission of the measurement signal.



Design description



houses the sensor

- different Base Plate materials (stainless steel or copper).

Thermal assessment of the final design

- Nuclear heat loads foreseen in stainless steel (200 kW/m³) underneath the blanket modules has been applied (with density scaling on other materials).
- Fillet welds considered, only thermal path toward the VV (water cooled at 100°C)
- Thermal contacts between Sensor Support and Base Plate only in the 4 bolting regions, to account for the high thermal contact resistance in vacuum
- \succ Temperature increase of 60°C in the full assembly and less than $3^{\circ}C$ in the sensor \rightarrow TIEMF well below 1 μ V (acceptable noise)

Electro-magnetic analysis

Sensor support structures shielding effect

- <u>Functional specifications</u>: $f_{cut-off}$ (-3 dB) > 15 kHz
- 3D harmonic magnetic FEM analyses

1st analysis set

<u>Aim</u>: to define shape and materials of sensor clamp brackets

Results: 'cross shaped support' made of copper

- minimized EM shielding effect
- still adequate thermal conductance (not achievable with SS)

2nd analysis set

Aim: to assess the EM shielding effect of the whole metallic structures around the sensor: clamp bracket, cradle and ECH shielding cover

Model: 1/4 of sensor assembly (exploits 2 symmetry planes)

<u>Results</u>: ECH shield dramatically reduces f_{cut-off} << 10 kHz; required sensor cover modification:

- 0.2 mm thickness SS cover
- or "metal coated ceramic" as for HF sensors.



craddle (Cu) + cover (0.5 mm - SS) - (no clamp) + craddle (Cu) + cover (0.5 mm - SS) clamp (Cu) + (no craddle) + (no cover)



clamp (Cu) + cradle (Cu) + cover (SS)





- allows its replacement by proper RH features
- made of copper to provide good thermal path (to limit overtemperature within the sensor due to nuclear heating)
- different configurations for different kinds of sensor
- specific features to prevent penetration of ECH stray radiation (labyrinth shaped interfaces and EMI shielding gaskets)
- suitable venting holes guarantee a proper vacuum pumping.

Connector Cover

- 3 mm thick Stainless Steel plate
- protects the electrical connector
- allows its replacement by proper RH features
- specific features prevent the penetration of ECH stray radiation

Structural analysis

Base Plate structural assessment (normal and off normal operation) Boundary conditions:

- gravity and seismic loads negligible (according to specifications);
- only worst EM forces, induced during fast discharge events, (max = 7.1 kN, assessed with proper EM calculations), and thermal loads considered. Assessment (according to the French nuclear norm RCC-MR):
- different load combinations classified;
- components verified against plastic collapse, ratcheting and fatigue.

Results: welds are the most critical parts:

- additional safety factors and strong fatigue life requirements limit the allowable stress in the welds (decided by ITER Organization);
- allowed primary membrane stress fixed at 14.1 MPa (1/10 of AISI 316L base material at 150°C) for fillet welds on VV (full inspection testing not possible);
- fatigue (nuclear heating secondary stress has to be considered) is not satisfied.
- Redesign of the Base Plate weld zone and the selection of full penetration welds, which allow higher allowable stress, is presently under consideration.

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